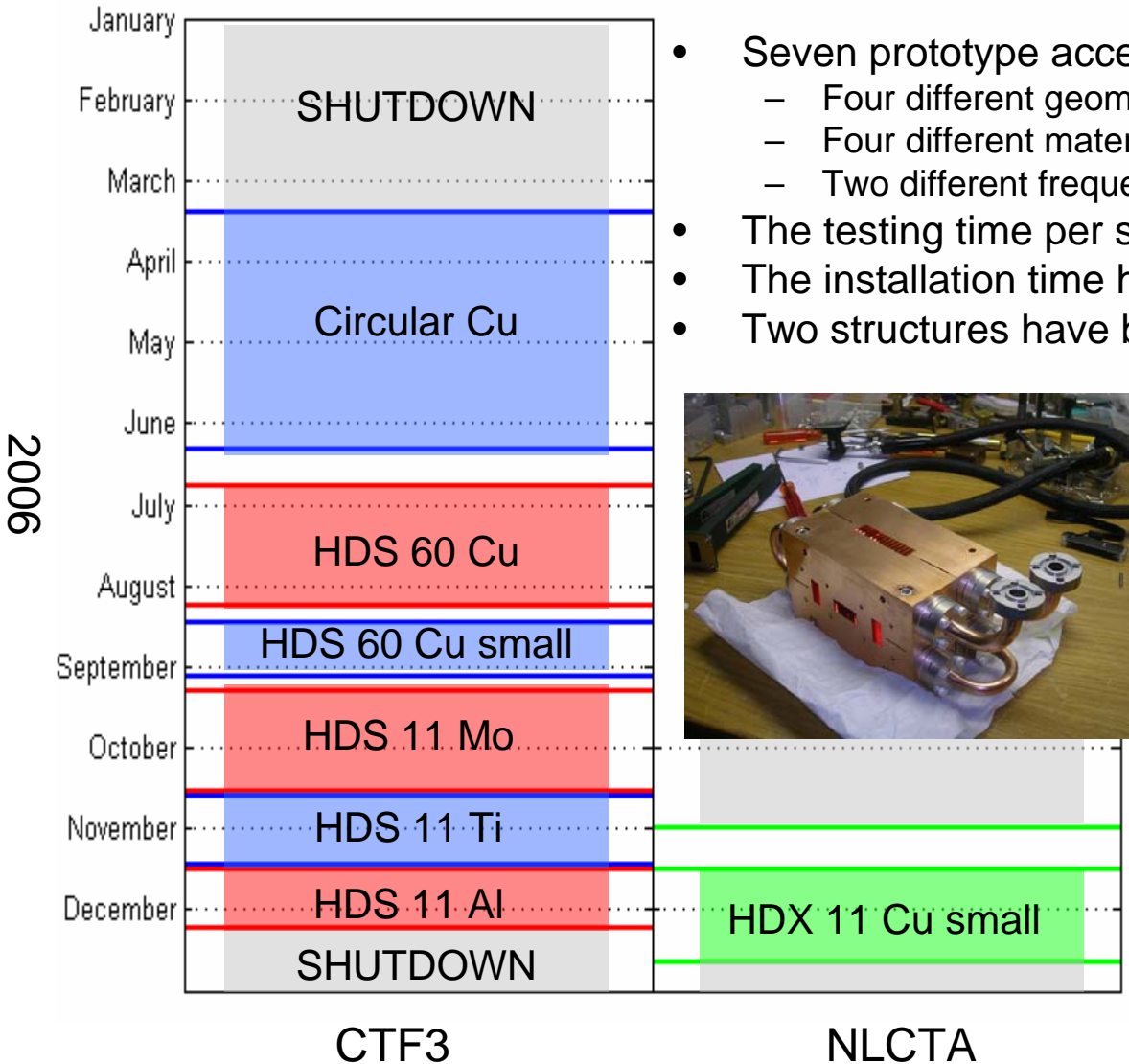


# Results from recent 30 GHz and X-band Accelerating Structure Tests

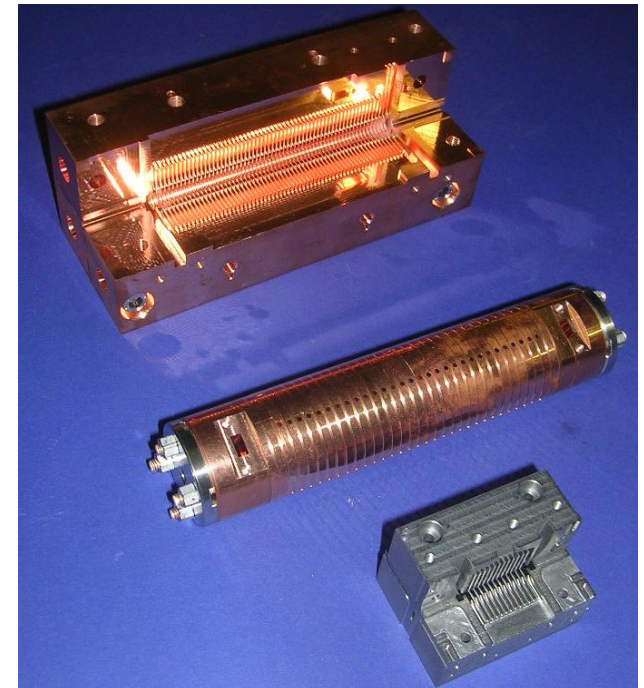
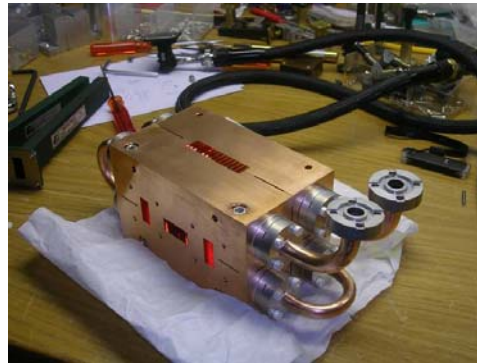
# Contents

- The Structures tested
- Material
- Frequency
- Breakdown rate
- Conclusions

# The Structures tested



- Seven prototype accelerating structures were tested:
  - Four different geometries (Circular, HDS 11, HDX 11, HDS 60)
  - Four different materials (Cu, Al, Ti, Mo)
  - Two different frequencies
- The testing time per structure has been reduced
- The installation time has also been reduced
- Two structures have been tested at the same time



# The Structures tested

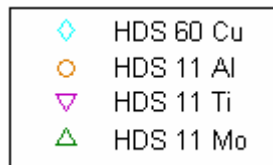
	HDS 11	HDS 60	HDS 60 Small	HDX 11 Small
Assembly	Clamped Quadrants			
Number of cells	11	60	60	11
$P_{INC}$ [MW] @ $E_{1st} = 150$ MV/m	98		54	370
$E_{SURFACE}$ [MV/m] @ $E_{1st} = 150$ MV/m	268		252	252
a [mm]	1.9		1.6	

Other Structures Tested	
30 GHz	2 x Circular Mo
	1 x Circular W
	2 x Circular Cu
11.4 GHz	1 x Circular Mo
	1 x Circular W

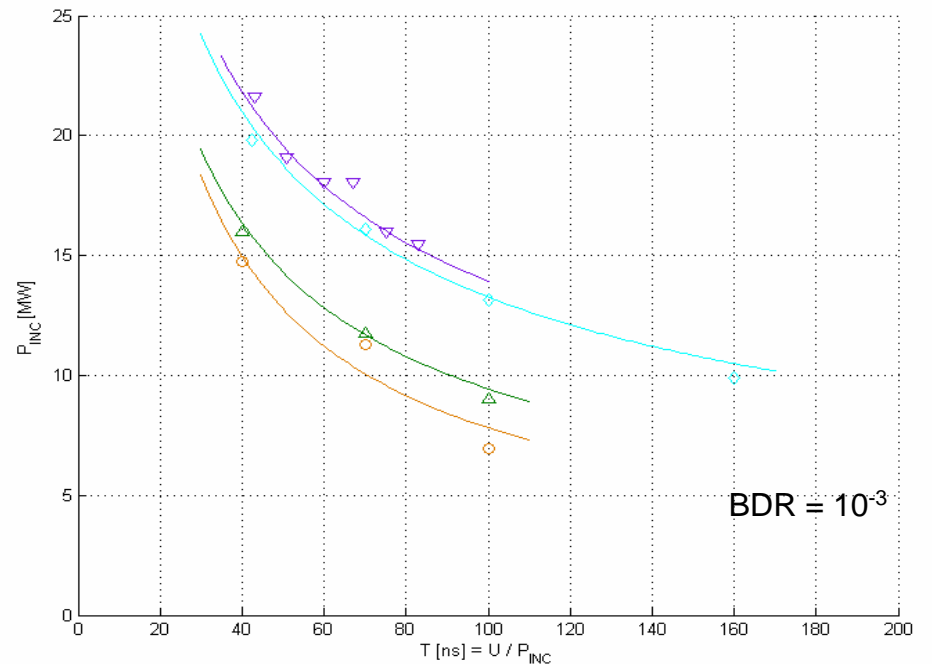
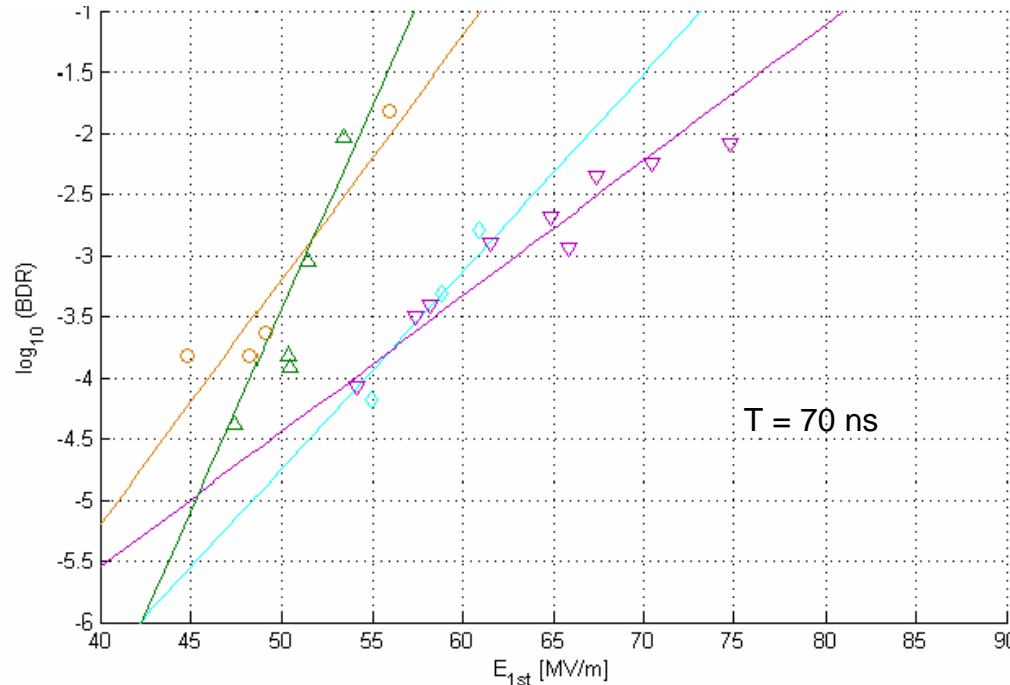
	Circular Structures @ 30 GHz
Assembly	Clamped or brazed cells
Number of cells	30
$P_{INC}$ [MW] @ $E_{1st} = 150$ MV/m	54
$E_{SURFACE}$ [MV/m] @ $E_{1st} = 150$ MV/m	330
a [mm]	1.75



# Material



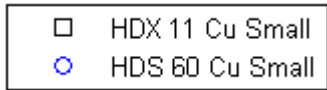
	HDS 11 Ti	HDS 60 Cu	HDS 11 Mo	HDS 11 Al
$E_{1st}$ [MV/m] @ 70ns, BDR= $10^{-3}$	63	61 (97%)	51 (81%)	51 (81%)
$E_{1st}$ [MV/m] @ 70ns, BDR= $10^{-6}$	36	42 (117%)	42 (117%)	36 (100%)
$P_{INC} / C$ [MW/mm] @ 70ns, BDR= $10^{-3}$	1.72	1.61 (94%)	1.13 (66%)	1.13 (66%)
$P_{INC} / C$ [MW/mm] @ 70ns, BDR= $10^{-6}$	0.56	0.76 (136%)	0.76 (136%)	0.56 (100%)
Slope [MV/decade]	9.0	6.2	3.0	5.0
$k$ in $P T^k = CTE$	-0.49	-0.50	-0.60	-0.71



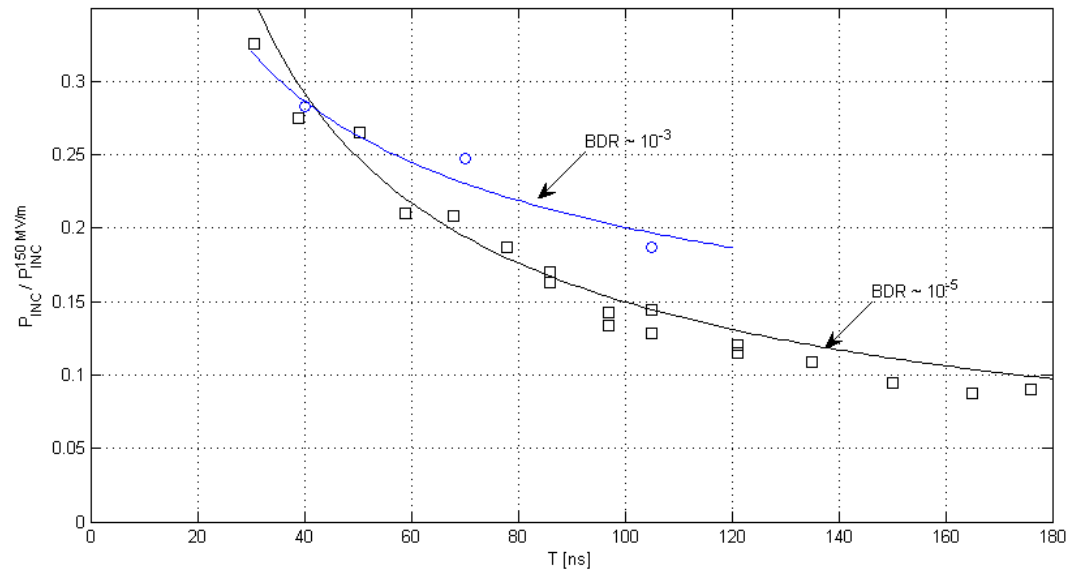
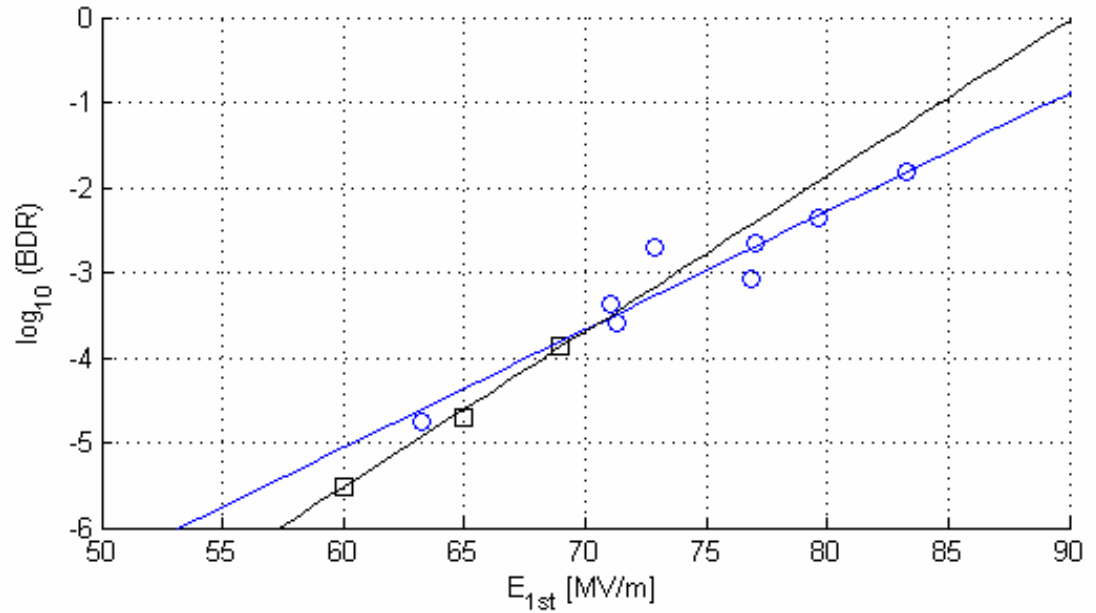
# Material

- Slopes seem to be different for different materials
- Therefore, the relative performance of the different materials depends on the desired breakdown rate
- In particular at  $BDR = 10^{-3}$  (well characterized experimentally), Ti is the best performer
- The performance of Ti could be even better than shown (a degradation of the performance was observed while conditioning)
- A different material ordering was observed in other experiments (brazed circular copper, clamped circular molybdenum)
- The pulse length dependence seems to be stronger than the traditional  $1/3$  even for copper
- The relative performance of the materials does not depend on the chosen pulse length (in the range it was measured)

# Frequency



	HDS 60 Cu Small	HDX 11 Cu Small
$E_{1st}$ [MV/m] @ 70ns, BDR= $10^{-3}$	75	74
$E_{1st}$ [MV/m] @ 70ns, BDR= $10^{-6}$	53	57
Slope [MV/decade]	7.2	5.5
$k$ in $P T^k = CTE$	-0.39	-0.73

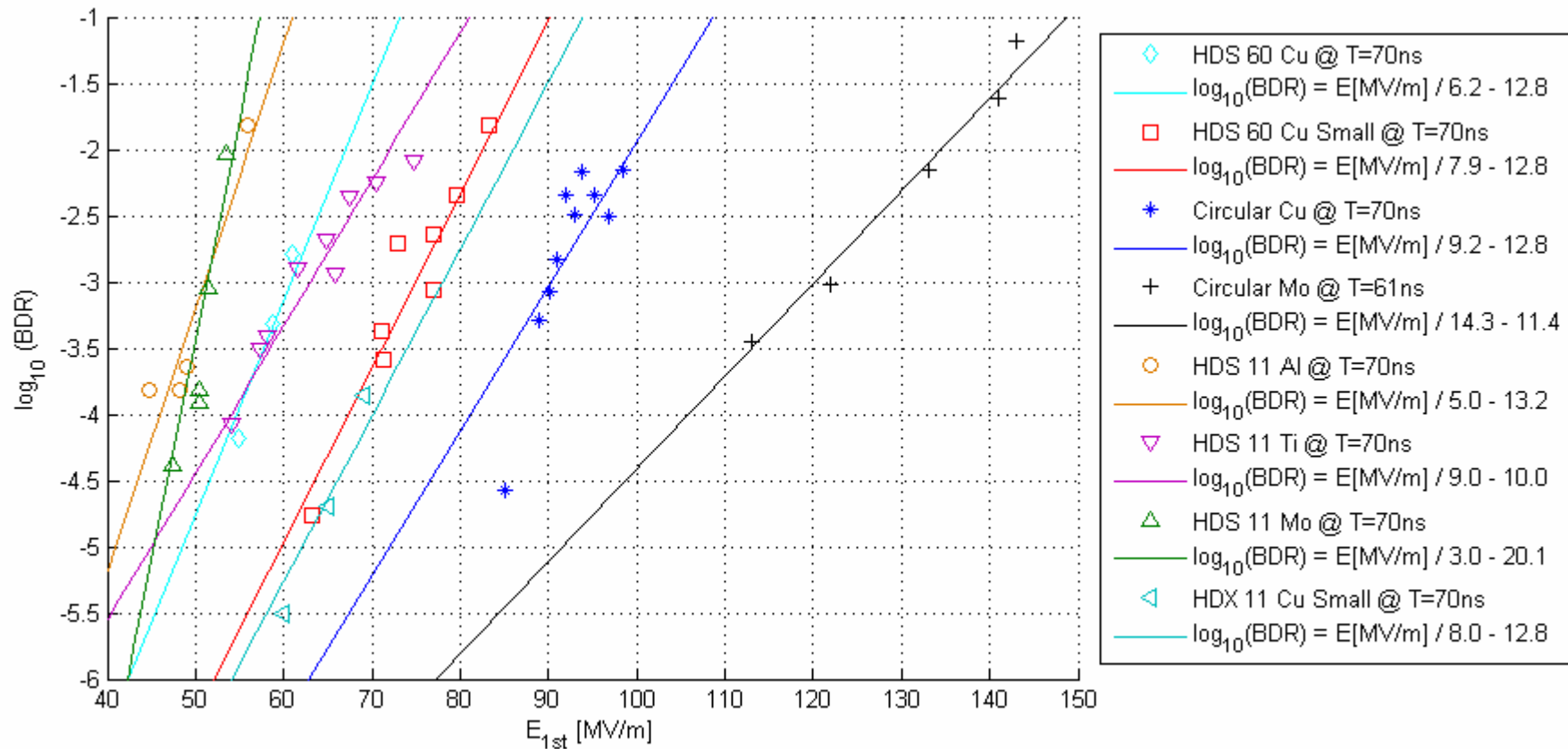


# Frequency

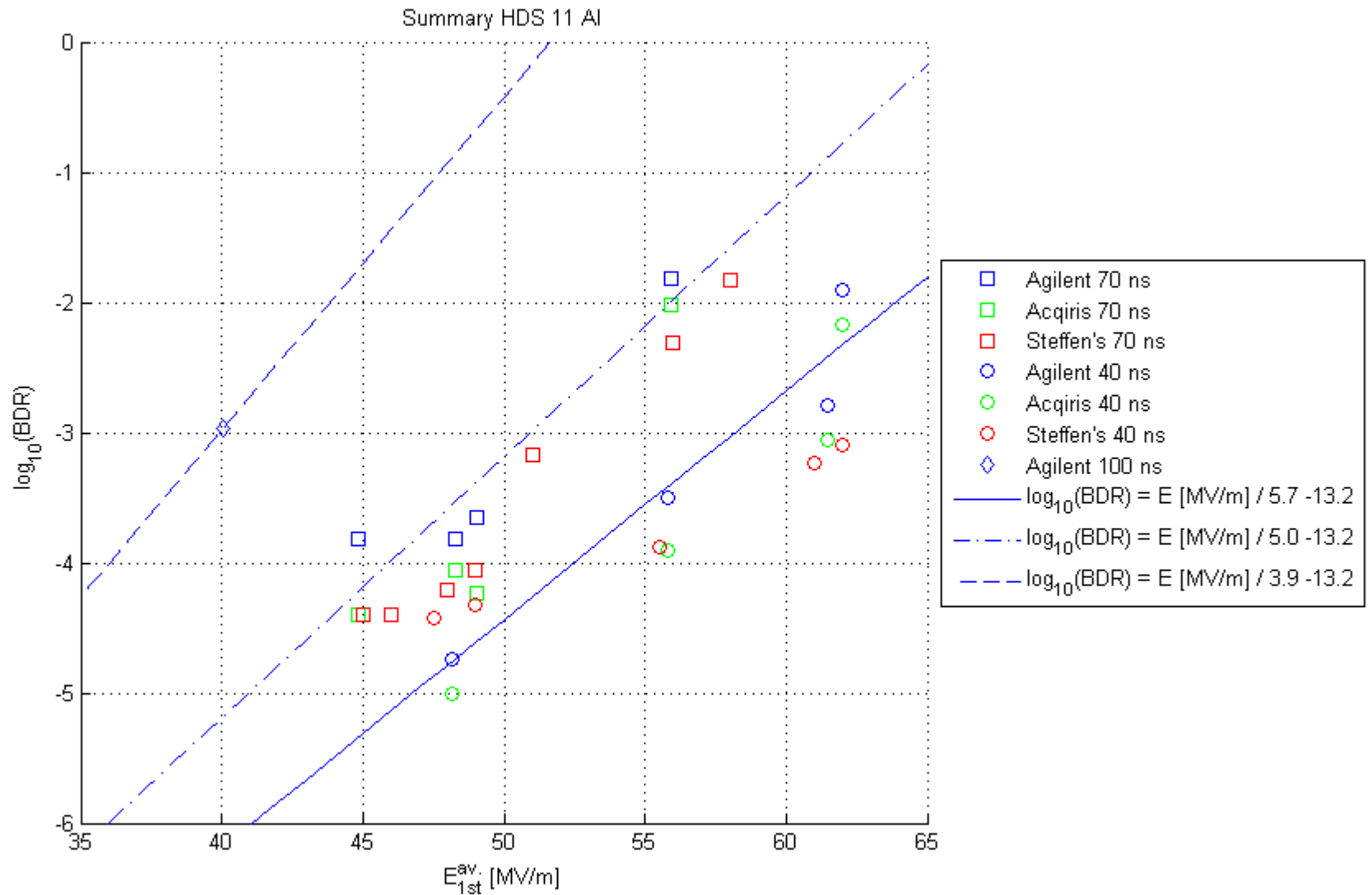
- Slopes are similar in both structures
- Two other pairs of similar structures have been tested before at different frequencies
- The pulse length dependence seems to be the traditional  $1/3$  in the 30 GHz structure but steeper in the 11.4 GHz structure
- A degradation of the HDX structure was observed during the conditioning that could also explain the stronger than usual pulse length dependence



# Breakdown rates @ 70 ns



# HDS 11 Al: Breakdown rates



# HDS 11 AI: Breakdown rates

## With free linear dependence @ 70ns

Linear model Poly1:

$$f(x) = p1*x + p2$$

Coefficients (with 95% confidence bounds):

$$p1 = 0.1966 \text{ } (-0.02601, 0.4193)$$

$$p2 = -13.02 \text{ } (-24.08, -1.953)$$

Goodness of fit:

SSE: 0.3464

R-square: 0.8783

Adjusted R-square: 0.8175

RMSE: 0.4162

## With free linear dependence @ 40ns

Linear model Poly1:

$$f(x) = p1*x + p2$$

Coefficients (with 95% confidence bounds):

$$p1 = 0.1789 \text{ } (0.02305, 0.3348)$$

$$p2 = -13.41 \text{ } (-22.31, -4.5)$$

Goodness of fit:

SSE: 0.3266

R-square: 0.9242

Adjusted R-square: 0.8863

RMSE: 0.4041

## With fixed (to the average of the two free fits) linear dependence @ 70ns

Linear model Poly1:

$$f(x) = p1*x + p2$$

Coefficients (with 95% confidence bounds):

$$p1 = 0.2006 \text{ } (0.1897, 0.2115)$$

$$p2 = -13.22 \text{ } (\text{fixed at bound})$$

Goodness of fit:

SSE: 0.3475

R-square: 0.878

Adjusted R-square: 0.878

RMSE: 0.3403

## With fixed (to the average of the two free fits) linear dependence @ 40ns

Linear model Poly1:

$$f(x) = p1*x + p2$$

Coefficients (with 95% confidence bounds):

$$p1 = 0.1756 \text{ } (0.1664, 0.1848)$$

$$p2 = -13.22 \text{ } (\text{fixed at bound})$$

Goodness of fit:

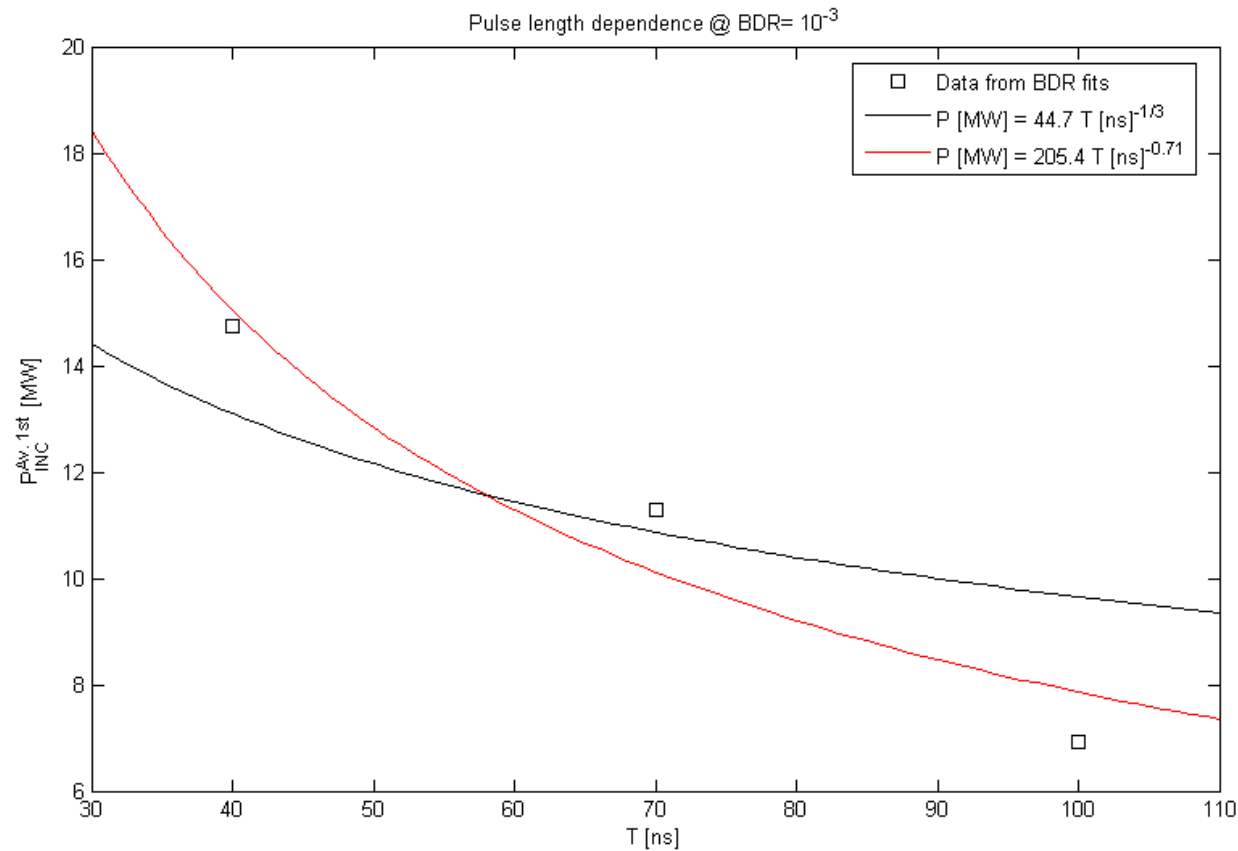
SSE: 0.3279

R-square: 0.9239

Adjusted R-square: 0.9239

RMSE: 0.3306

# HDS 11 AI: Pulse length dependence



# HDS 11 AI: Pulse length dependence

## With fixed power dependence 1/3

General model Power1:

$$f(x) = a \cdot x^b$$

Coefficients (with 95% confidence bounds):

$$a = 44.72 \quad (22.46, 66.99)$$

$$b = -0.333 \quad (\text{fixed at bound})$$

Goodness of fit:

SSE: 10.25

R-square: 0.6648

Adjusted R-square: 0.6648

RMSE: 2.263

## With free power dependence

General model Power1:

$$f(x) = a \cdot x^b$$

Coefficients (with 95% confidence bounds):

$$a = 205.4 \quad (-2026, 2437)$$

$$b = -0.7086 \quad (-3.427, 2.01)$$

Goodness of fit:

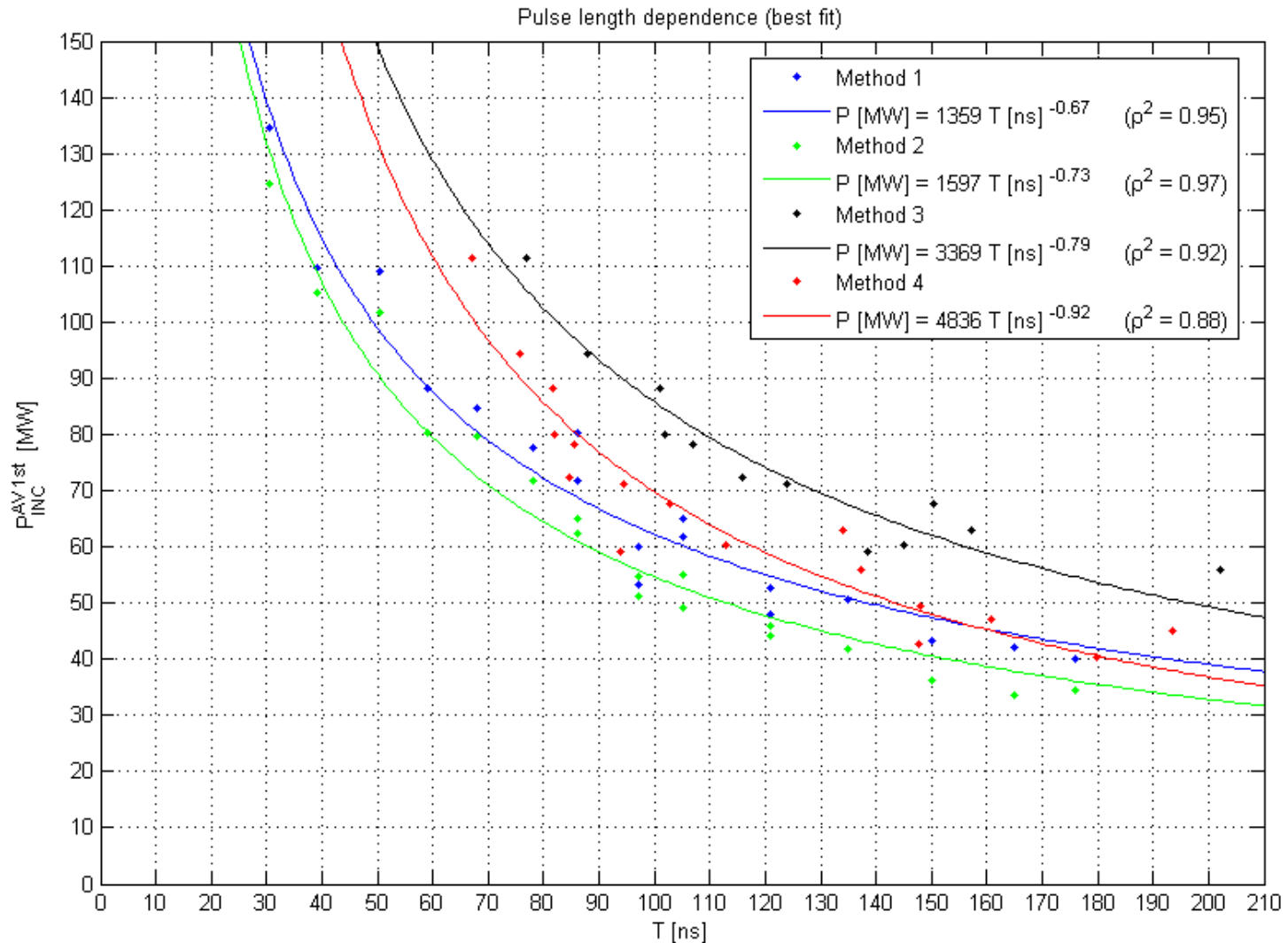
SSE: 2.322

R-square: 0.924

Adjusted R-square: 0.8481

RMSE: 1.524

# HDX 11 Cu: Pulse length dependence

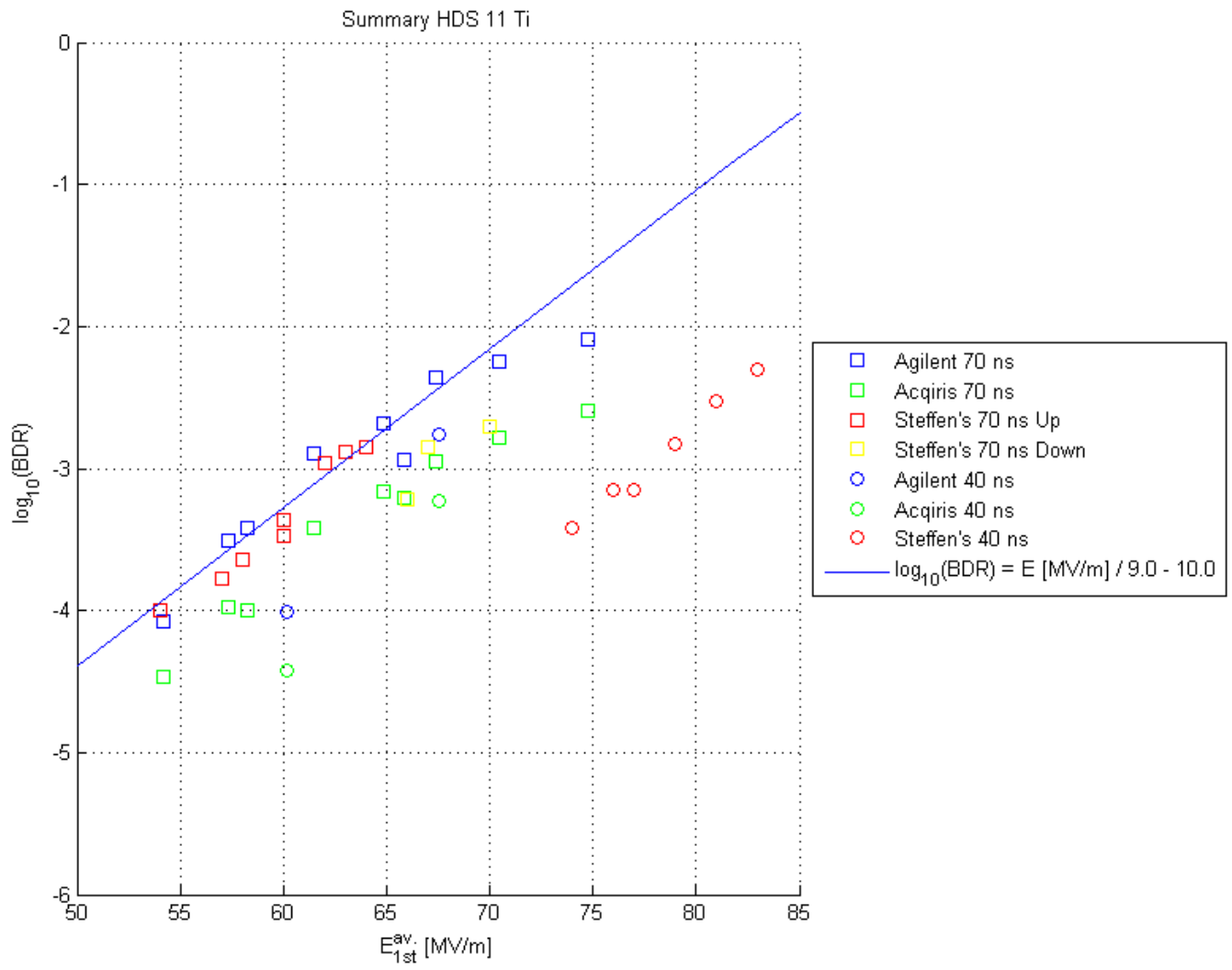


# Pulse length dependence measurements

## Description of different measurements

- **Tscope\_1, Vmax\_1, Vtop\_1:**
  - The pulse length (Tscope\_1) was changed from 30.5 ns to 176 ns. Note that all the pulse lengths used are those automatically measured by the scope in the control room.
  - For each pulse length, the power was slowly ramped up until a breakdown occurred (typically it took ~ 1 minute each time the power was ramped up).
  - At that point, the power was reduced without changing the pulse length and after waiting for 20 seconds before putting power in the structure.
  - This process was repeated for 15 minutes without taking any data.
  - Afterwards, five more ramp ups were performed writing down the maximum power read by the peak power meters (Vmax, Vtop)
  - Vmax\_1 and Vtop\_1 are the maximum values read by the peak power meters in those five ramp ups.
- **Tscope\_2, Vmax\_2, Vtop\_2:**
  - Vmax\_2 and Vtop\_2 are the average values read by the peak power meters in the five ramp ups described before.
- **Tscope\_3, Vmax\_3, Vtop\_3:**
  - The power (Vtop\_3) was changed from 54.5 MW to 134.5 MW. Note that the lowest power was defined by the maximum pulse length reachable without deteriorating the pulse shape (~200 ns).
  - For each power, the pulse length was ramped up until a breakdown occurred (typically it took ~ 1 minute each time the pulse length was ramped up).
  - At that point, the pulse length was reduced without changing the power and after waiting for 20 seconds before putting power in the structure.
  - This process was repeated for 15 minutes without taking any data.
  - Afterwards, ten more ramp ups were performed writing down the maximum pulse length read by the scope (Tscope)
  - Tscope\_3 is the maximum value read in those ten ramp ups.
- **Tscope\_4, Vmax\_4, Vtop\_4:**
  - Tscope\_4 is the average value read in the ten ramp ups described before.

# HDS 11 Ti: Breakdown rates





# HDS 11 Ti: Breakdown rates

With free linear dependence and excluding  
the two points with the highest BDR @ 70ns

Linear model Poly1:

$$f(x) = p1*x + p2$$

Coefficients (with 95% confidence bounds):

$$p1 = 0.1114 (0.07064, 0.1522)$$

$$p2 = -9.956 (-12.46, -7.448)$$

Goodness of fit:

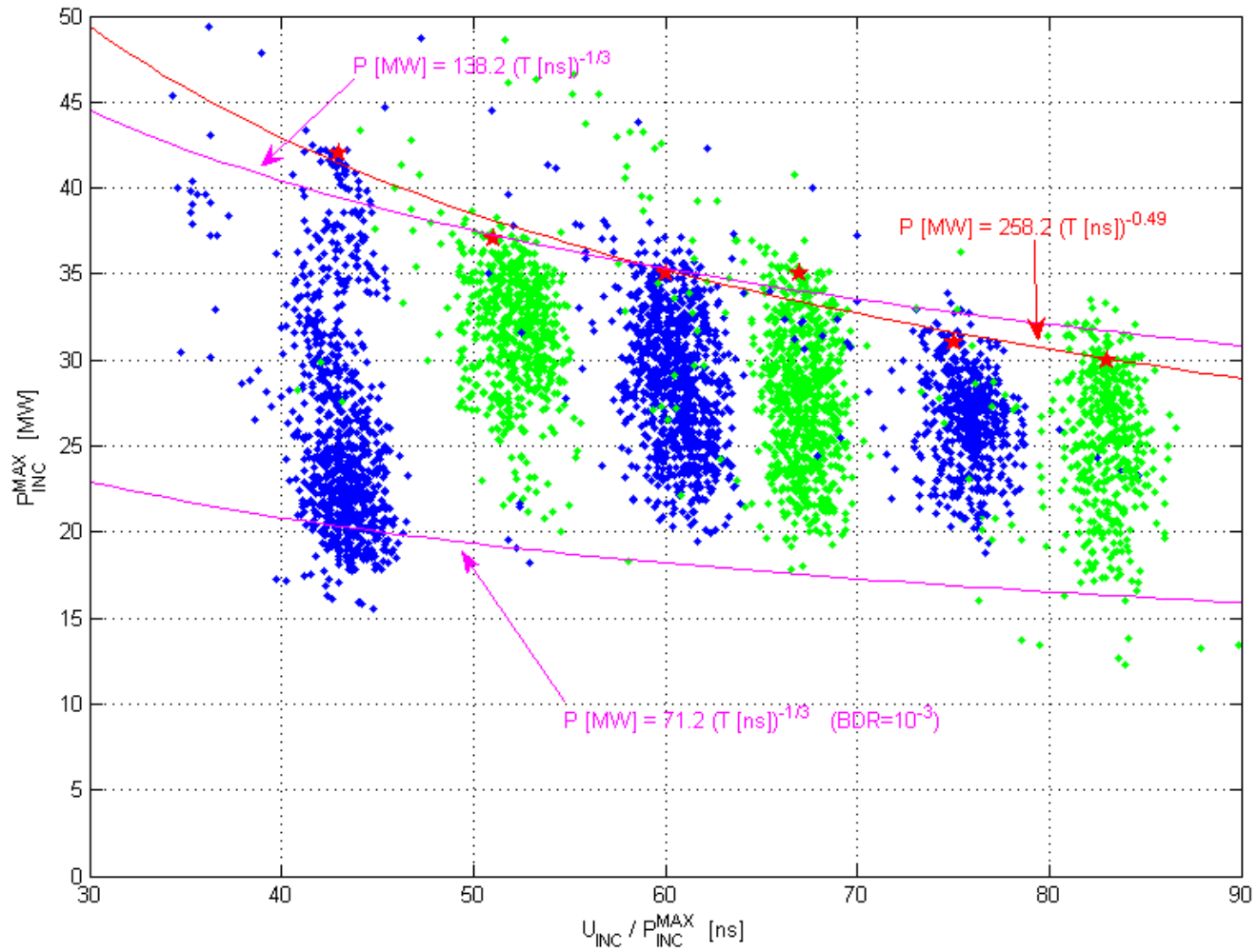
SSE: 0.1845

R-square: 0.908

Adjusted R-square: 0.8896

RMSE: 0.1921

# HDS 11 Ti: Pulse length dependence



# HDS 11 Ti: Pulse length dependence

## With fixed power dependence 1/3

General model Power1:

$$f(x) = a \cdot x^b$$

Coefficients (with 95% confidence bounds):

$$a = 138.2 \quad (131.4, 145)$$

$$b = -0.3333 \quad (\text{fixed at bound})$$

Goodness of fit:

SSE: 13.59

R-square: 0.8554

Adjusted R-square: 0.8554

RMSE: 1.649

## With free power dependence

General model Power1:

$$f(x) = a \cdot x^b$$

Coefficients (with 95% confidence bounds):

$$a = 258.2 \quad (97.9, 418.6)$$

$$b = -0.4864 \quad (-0.6386, -0.3341)$$

Goodness of fit:

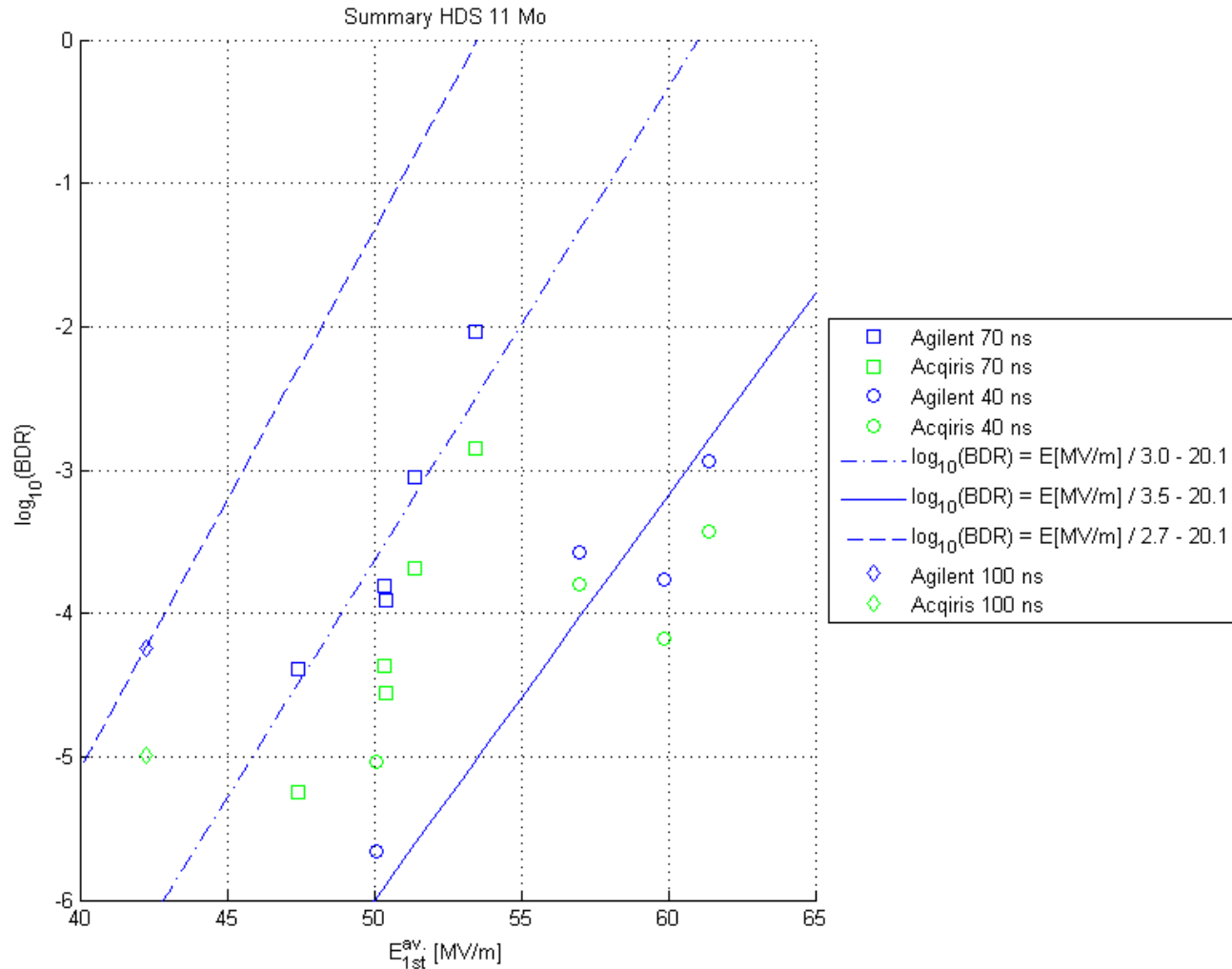
SSE: 4.621

R-square: 0.9508

Adjusted R-square: 0.9386

RMSE: 1.075

# HDS 11 Mo: Breakdown rates



# HDS 11 Mo: Breakdown rates

With free linear dependence @ 70ns

Linear model Poly1:

$$f(x) = p1*x + p2$$

Coefficients (with 95% confidence bounds):

$$p1 = 0.3984 (0.129, 0.6678)$$

$$p2 = -23.6 (-37.25, -9.957)$$

Goodness of fit:

SSE: 0.4041

R-square: 0.8807

Adjusted R-square: 0.8409

RMSE: 0.367

With free linear dependence @ 40ns

Linear model Poly1:

$$f(x) = p1*x + p2$$

Coefficients (with 95% confidence bounds):

$$p1 = 0.2224 (0.009202, 0.4355)$$

$$p2 = -16.68 (-28.88, -4.474)$$

Goodness of fit:

SSE: 0.3726

R-square: 0.9097

Adjusted R-square: 0.8645

RMSE: 0.4316

With fixed (to the average of the two free fits) linear dependence @ 70ns

Linear model Poly1:

$$f(x) = p1*x + p2$$

Coefficients (with 95% confidence bounds):

$$p1 = 0.3301 (0.3215, 0.3387)$$

$$p2 = -20.14 \text{ (fixed at bound)}$$

Goodness of fit:

SSE: 0.4919

R-square: 0.8548

Adjusted R-square: 0.8548

RMSE: 0.3507

With fixed (to the average of the two free fits) linear dependence @ 40ns

Linear model Poly1:

$$f(x) = p1*x + p2$$

Coefficients (with 95% confidence bounds):

$$p1 = 0.2827 (0.2698, 0.2956)$$

$$p2 = -20.14 \text{ (fixed at bound)}$$

Goodness of fit:

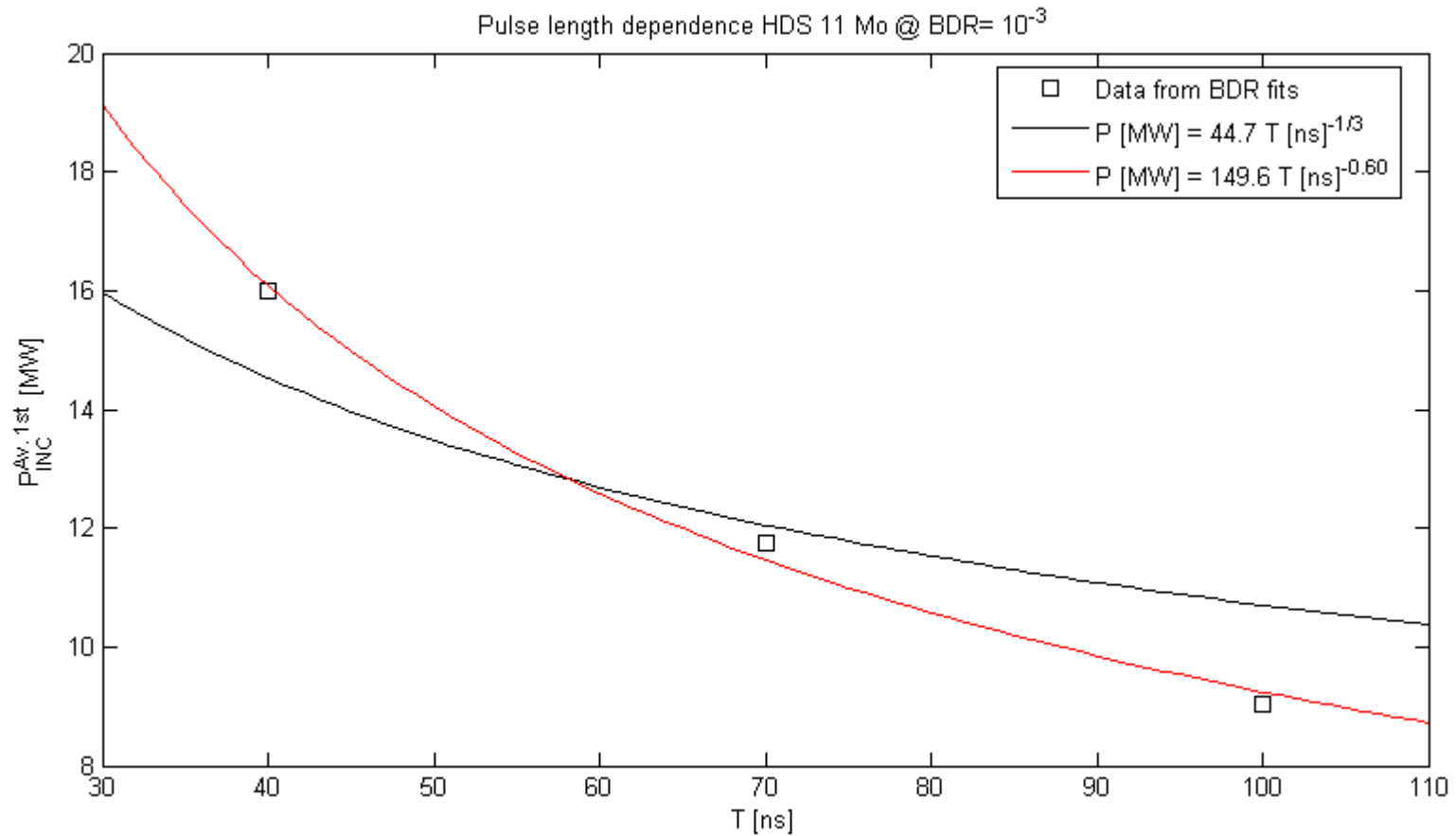
SSE: 0.6503

R-square: 0.8424

Adjusted R-square: 0.8424

RMSE: 0.4656

# HDS 11 Mo: Pulse length dependence



# HDS 11 Mo: Pulse length dependence

## With fixed power dependence 1/3

General model Power1:

$$f(x) = a \cdot x^b$$

Coefficients (with 95% confidence bounds):

$$a = 49.66 \quad (33.97, 65.36)$$

$$b = -0.3333 \quad (\text{fixed at bound})$$

Goodness of fit:

SSE: 5.078

R-square: 0.7946

Adjusted R-square: 0.7946

RMSE: 1.593

## With free power dependence

General model Power1:

$$f(x) = a \cdot x^b$$

Coefficients (with 95% confidence bounds):

$$a = 149.6 \quad (-187.2, 486.5)$$

$$b = -0.6046 \quad (-1.164, -0.04526)$$

Goodness of fit:

SSE: 0.1248

R-square: 0.9949

Adjusted R-square: 0.9899

RMSE: 0.3533