

$m_N$ (GeV)	$p_T^{\ell_1}$ (GeV)	$p_T^{\ell_2}$ (GeV)	$m(\ell^\pm \ell^\pm W_{\text{jet}})$ (GeV)	$m(\ell W_{\text{jet}})$ (GeV)	$(p_T^{\text{miss}})^2/S_T$ (GeV)	Total bkgd.	$N_{\text{obs}}$	DY $A\epsilon$ (%)	VBF $A\epsilon$ (%)
<b><math>\mu\mu</math> channel SR1</b>									
85	>25	>10	>90	40–100	<9	$26.0 \pm 6.3$	30	$0.50 \pm 0.05$	—
90	>25	>10	>90	45–105	<9	$34.5 \pm 7.5$	35	$1.2 \pm 0.1$	—
100	>25	>15	>110	55–115	<9	$18.6 \pm 4.2$	20	$2.6 \pm 0.2$	—
125	>25	>25	>140	85–140	<7	$11.7 \pm 2.7$	12	$5.1 \pm 0.4$	—
150	>35	>35	>150	110–170	<7	$8.9 \pm 1.9$	11	$6.6 \pm 0.5$	—
200	>50	>40	>250	160–215	<7	$4.6 \pm 1.2$	4	$8.1 \pm 0.6$	—
250	>85	>45	>310	215–270	<7	$3.0 \pm 0.9$	2	$11.0 \pm 0.8$	—
300	>100	>50	>370	225–340	<7	$2.6 \pm 1.0$	2	$13.2 \pm 0.9$	$5.2 \pm 0.4$
400	>110	>60	>490	295–490	<7	$0.9 \pm 0.4$	3	$11.7 \pm 0.8$	$5.1 \pm 0.4$
500	>110	>60	>610	370–550	<7	$0.4^{+0.6}_{-0.4}$	3	$8.6 \pm 0.6$	$4.1 \pm 0.3$
600	>110	—	>680	370–630	<7	$0.3^{+0.3}_{-0.3}$	3	$7.4 \pm 0.5$	$4.1 \pm 0.3$
700	>110	—	>800	370–885	<7	$0.2^{+0.4}_{-0.2}$	2	$6.7 \pm 0.4$	$3.9 \pm 0.3$
800	>110	—	>800	370–890	<7	$0.2^{+0.4}_{-0.2}$	2	$6.0 \pm 0.4$	$5.4 \pm 0.3$
900	>110	—	>800	370–1225	<7	$0.3^{+0.4}_{-0.3}$	2	$5.4 \pm 0.4$	$5.0 \pm 0.3$
1000	>110	—	>800	370–1230	<7	$0.3^{+0.4}_{-0.3}$	2	$4.6 \pm 0.3$	$4.2 \pm 0.3$
1100	>110	—	>800	370–1245	<7	$0.3^{+0.4}_{-0.3}$	2	$4.1 \pm 0.3$	$3.8 \pm 0.3$
1200	>110	—	>800	370–1690	<7	$0.3^{+0.4}_{-0.3}$	2	$3.6 \pm 0.2$	$3.4 \pm 0.3$
1300	>110	—	>800	370–1890	<7	$0.3^{+0.4}_{-0.3}$	2	$3.2 \pm 0.2$	$3.0 \pm 0.2$
1400	>110	—	>800	370–1940	<7	$0.3^{+0.4}_{-0.3}$	2	$2.7 \pm 0.2$	$2.7 \pm 0.2$
1500	>110	—	>800	370–2220	<7	$0.3^{+0.4}_{-0.3}$	2	$2.5 \pm 0.2$	$2.3 \pm 0.2$
<b><math>\mu\mu</math> channel SR2</b>									
85	>25	>10	—	—	<15	$11.4 \pm 3.5$	13	$0.001 \pm 0.001$	—
90	>25	>10	—	90–170	<15	$4.1 \pm 1.3$	4	$0.003 \pm 0.003$	—
100	>25	>15	—	98–145	<15	$1.0 \pm 0.3$	0	$0.006 \pm 0.003$	—
125	>60	>15	—	110–150	<15	$0.8 \pm 0.3$	0	$0.08 \pm 0.01$	—
150	>70	>15	—	145–175	<15	$1.0 \pm 0.4$	2	$0.28 \pm 0.04$	—
200	>100	>20	—	175–235	<15	$1.3 \pm 0.8$	0	$1.4 \pm 0.1$	—
250	>140	>25	—	226–280	<15	$0.3 \pm 0.2$	0	$3.0 \pm 0.3$	—
300	>140	>40	—	280–340	<15	$0.4 \pm 0.3$	0	$5.4 \pm 0.5$	$0.7 \pm 0.1$
400	>140	>65	—	340–445	<15	$0.5 \pm 0.3$	2	$13.3 \pm 1.3$	$2.7 \pm 0.3$
500	>140	>65	—	445–560	<15	$0.8 \pm 0.5$	0	$22.4 \pm 2.2$	$6.8 \pm 0.7$
600	>140	—	—	560–685	<15	$0.7 \pm 0.4$	0	$30.2 \pm 2.9$	$20.4 \pm 1.8$
700	>140	—	—	635–825	<15	$0.8 \pm 0.4$	2	$34.6 \pm 3.4$	$24.7 \pm 2.2$
800	>140	—	—	755–960	<15	$0.4 \pm 0.3$	0	$34.8 \pm 3.5$	$24.9 \pm 2.3$
900	>140	—	—	840–1055	<15	$0.2^{+0.2}_{-0.2}$	1	$35.8 \pm 3.6$	$26.9 \pm 2.5$
1000	>140	—	—	900–1205	<15	$0.1^{+0.2}_{-0.1}$	1	$38.4 \pm 3.9$	$28.9 \pm 2.7$
1100	>140	—	—	990–1250	<15	$0.1^{+0.1}_{-0.1}$	1	$36.7 \pm 3.7$	$29.2 \pm 2.7$
1200	>140	—	—	1035–1430	<15	$0.2^{+0.3}_{-0.2}$	1	$38.5 \pm 4.0$	$30.1 \pm 2.8$
1300	>140	—	—	1100–1595	<15	$0.3 \pm 0.3$	1	$38.5 \pm 4.0$	$30.7 \pm 3.0$
1400	>140	—	—	1285–1700	<15	$0.1^{+0.2}_{-0.1}$	1	$35.9 \pm 3.8$	$29.4 \pm 2.8$
1500	>140	—	—	1330–1800	<15	$0.1^{+0.2}_{-0.1}$	1	$36.4 \pm 3.9$	$30.0 \pm 2.9$