

| $0.10 < q^2 < 0.98 \text{ GeV}^2/c^4$ | $1.1 < q^2 < 2.5 \text{ GeV}^2/c^4$ | $2.5 < q^2 < 4.0 \text{ GeV}^2/c^4$ | $4.0 < q^2 < 6.0 \text{ GeV}^2/c^4$ | $6.0 < q^2 < 8.0 \text{ GeV}^2/c^4$ | $11.0 < q^2 < 12.5 \text{ GeV}^2/c^4$ | $15.0 < q^2 < 17.0 \text{ GeV}^2/c^4$ | $17.0 < q^2 < 19.0 \text{ GeV}^2/c^4$ | $1.1 < q^2 < 6.0 \text{ GeV}^2/c^4$ | $15.0 < q^2 < 19.0 \text{ GeV}^2/c^4$ | | | | | | | | | | |
|---------------------------------------|-------------------------------------|-------------------------------------|-------------------------------------|-------------------------------------|---------------------------------------|---------------------------------------|---------------------------------------|-------------------------------------|---------------------------------------|----------|------------------------------|----------|------------------------------|----------|------------------------------|----------|------------------------------|----------|------------------------------|
| F_L | $0.255 \pm 0.032 \pm 0.007$ | F_L | $0.655 \pm 0.046 \pm 0.017$ | F_L | $0.756 \pm 0.047 \pm 0.023$ | F_L | $0.684 \pm 0.035 \pm 0.015$ | F_L | $0.645 \pm 0.030 \pm 0.011$ | F_L | $0.461 \pm 0.031 \pm 0.010$ | F_L | $0.352 \pm 0.026 \pm 0.009$ | F_L | $0.344 \pm 0.032 \pm 0.025$ | F_L | $0.700 \pm 0.025 \pm 0.013$ | F_L | $0.345 \pm 0.020 \pm 0.007$ |
| S_3 | $0.034 \pm 0.044 \pm 0.003$ | S_3 | $-0.107 \pm 0.052 \pm 0.003$ | S_3 | $0.020 \pm 0.053 \pm 0.002$ | S_3 | $0.014 \pm 0.038 \pm 0.003$ | S_3 | $-0.013 \pm 0.038 \pm 0.004$ | S_3 | $-0.124 \pm 0.037 \pm 0.003$ | S_3 | $-0.166 \pm 0.034 \pm 0.007$ | S_3 | $-0.250 \pm 0.050 \pm 0.025$ | S_3 | $-0.012 \pm 0.025 \pm 0.003$ | S_3 | $-0.189 \pm 0.030 \pm 0.009$ |
| S_4 | $0.059 \pm 0.050 \pm 0.004$ | S_4 | $-0.038 \pm 0.070 \pm 0.011$ | S_4 | $-0.187 \pm 0.074 \pm 0.008$ | S_4 | $-0.145 \pm 0.057 \pm 0.004$ | S_4 | $-0.275 \pm 0.045 \pm 0.006$ | S_4 | $-0.245 \pm 0.047 \pm 0.007$ | S_4 | $-0.299 \pm 0.033 \pm 0.008$ | S_4 | $-0.307 \pm 0.041 \pm 0.008$ | S_4 | $-0.136 \pm 0.039 \pm 0.003$ | S_4 | $-0.303 \pm 0.024 \pm 0.008$ |
| S_5 | $0.227 \pm 0.041 \pm 0.008$ | S_5 | $0.174 \pm 0.060 \pm 0.007$ | S_5 | $-0.064 \pm 0.068 \pm 0.010$ | S_5 | $-0.204 \pm 0.051 \pm 0.013$ | S_5 | $-0.279 \pm 0.043 \pm 0.013$ | S_5 | $-0.310 \pm 0.043 \pm 0.011$ | S_5 | $-0.341 \pm 0.034 \pm 0.009$ | S_5 | $-0.280 \pm 0.040 \pm 0.014$ | S_5 | $-0.052 \pm 0.034 \pm 0.007$ | S_5 | $-0.317 \pm 0.024 \pm 0.011$ |
| A_{FB} | $-0.004 \pm 0.040 \pm 0.004$ | A_{FB} | $-0.229 \pm 0.046 \pm 0.009$ | A_{FB} | $-0.070 \pm 0.043 \pm 0.006$ | A_{FB} | $0.050 \pm 0.033 \pm 0.002$ | A_{FB} | $0.110 \pm 0.027 \pm 0.005$ | A_{FB} | $0.333 \pm 0.030 \pm 0.008$ | A_{FB} | $0.385 \pm 0.024 \pm 0.007$ | A_{FB} | $0.323 \pm 0.032 \pm 0.019$ | A_{FB} | $-0.073 \pm 0.021 \pm 0.002$ | A_{FB} | $0.353 \pm 0.020 \pm 0.010$ |
| S_7 | $0.006 \pm 0.042 \pm 0.002$ | S_7 | $-0.107 \pm 0.063 \pm 0.004$ | S_7 | $-0.066 \pm 0.065 \pm 0.004$ | S_7 | $-0.136 \pm 0.053 \pm 0.002$ | S_7 | $-0.074 \pm 0.046 \pm 0.003$ | S_7 | $-0.096 \pm 0.050 \pm 0.003$ | S_7 | $0.029 \pm 0.039 \pm 0.001$ | S_7 | $0.049 \pm 0.049 \pm 0.007$ | S_7 | $-0.090 \pm 0.034 \pm 0.002$ | S_7 | $0.035 \pm 0.030 \pm 0.003$ |
| S_8 | $-0.003 \pm 0.051 \pm 0.001$ | S_8 | $-0.174 \pm 0.075 \pm 0.002$ | S_8 | $0.016 \pm 0.074 \pm 0.002$ | S_8 | $0.077 \pm 0.062 \pm 0.001$ | S_8 | $-0.062 \pm 0.047 \pm 0.001$ | S_8 | $0.009 \pm 0.049 \pm 0.001$ | S_8 | $0.003 \pm 0.042 \pm 0.002$ | S_8 | $-0.026 \pm 0.046 \pm 0.002$ | S_8 | $-0.009 \pm 0.037 \pm 0.002$ | S_8 | $0.005 \pm 0.031 \pm 0.001$ |
| S_9 | $-0.055 \pm 0.041 \pm 0.002$ | S_9 | $-0.112 \pm 0.054 \pm 0.005$ | S_9 | $-0.012 \pm 0.055 \pm 0.003$ | S_9 | $0.029 \pm 0.045 \pm 0.002$ | S_9 | $0.024 \pm 0.035 \pm 0.002$ | S_9 | $0.042 \pm 0.040 \pm 0.003$ | S_9 | $0.000 \pm 0.037 \pm 0.002$ | S_9 | $-0.056 \pm 0.045 \pm 0.002$ | S_9 | $-0.025 \pm 0.026 \pm 0.002$ | S_9 | $-0.031 \pm 0.029 \pm 0.001$ |